FLOOD ESTIMATE USING GIS SPECIFIC TO FLOOD STUDIES FOR UPPER SARADA RIVER BASIN IN VISAKHAPATNAM DISTRICT, ANDHRA PRADESH, INDIA

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Abstract

Geographical Information System (GIS) techniques have been effectively used for the study of drainages and estimation of runoff of a catchment. In this paper, the flood estimate of the Upper Sarada River Basin is analyzed using GIS techniques. The Upper Sarada River Basin is analyzed by building a Drainage Elevation Model and thereby extracting the drainage map. The runoff is estimated on this catchment by assuming unit net rainfall (1cm direct runoff) and taking appropriate assumptions. For this purpose, streams in a River Basin are assigned weights with respect to slope of the area and using the same, a travel time contour map represented by isochrones is developed from the equivalent distance map. The flow accumulation map of the drainages is also developed and then this is used to determine discharge at outlet of the catchment. The entire basin area is divided into eleven parts of equal interval of travel time and the yield caused in each part is determined. Further, this is used to determine the discharge at the end of eleven-time steps and the resulting unit hydrograph (UH) is plotted. UH is prepared for the daily average run-off values. An S-hydrograph is also plotted to obtain a UH of selected time duration for the use in flood estimate due to a storm. This hydrograph is validated by taking different selected storm events from the year 1990 to 2019, recorded by Central Water Commission (CWC), Anakapalle station. Eight storm events are observed and these are validated using Thiessen polygon method.

Keywords: DEM, Runoff, Catchment, Isochrones, Unit Hydrograph, Flood estimation and Thiessen polygon map.

INTRODUCTION

The nature of stream flow in any region is related to rainfall characteristics and the morphology of the watershed. The rainfall characteristics include the intensity and volume of rainfall and its spatial and temporal distribution. The study of the hydrological characteristics of the basins and development of mathematical models for rainfall and runoff relationships that bind it with the topographic characteristics was first made by Sherman(1932). The geomorphic characteristics are the channel network and the surrounding landscape, which translate the rainfall input into an output hydrograph at the outlet of the watershed (Berihun et al. 2019). An unusual high state of the river flow due to excess runoff from rainfall produces flood. The maximum flood discharge (peak runoff) in a river may be determined by different methods(Zhu & Hao, 2014). They are empirical formulae and curves, concentration time method, overland flow hydrograph, rational method, unit hydrograph method and flood frequency studies(Sreedevi et al. 2013; Vijay P. Singh, 1988). One of the above methods, flood estimation by unit hydrograph method is mostly used for catchments having areas less than 5000 km²(Arnold et al. 1998;Destaet al. 2019). In the recent times, digital elevation model (DEM) based unit hydrograph using Geographic Information System (GIS) has gained importance as an effective tool for the analysis of spatial, non-spatial data on drainage, geology, landform parameters and to understand their interrelationships(Debala Devi & Usha Anandhi, 2009; Maathuis & Wang; 2006, Moore et al. 1991; Noto & La Loggia, 2007).

LITERATURE REVIEW

DEMs are most widely used in the watershed modeling. The automatic derivation of topographic watershed data from DEM is faster, less subjective and provides more reproducible measurements than the traditional manual techniques applied using the topographic maps(Patel & Sarkar ,2010).

The technological advances provided by GIS and the increasing availability and high quality DEMs have greatly expanded the application potential of DEMs in many hydrologic, hydraulic, water resources and environmental investigations(Moore et al. 1991; Singh et al. 2014). The DEM provides a basic spatial reference system to the GIS spatial data. Images or vector information can automatically be draped over and integrated with the DEM for more advanced analysis(Lau et al. 2010). Effective process for drainage network identification based on DEMs by conducting a comparative analysis of various geomorphologic

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characteristics. In India, DEMs have been employed for River Basin analysis, estimation of soil loss, water resource evaluation and topographic characterization by various hydrologists(Agarwal et al. 2012; Aher et al. 2014; Patel & Sarkar, 2010).

Rational method is a popular technique developed to predict peak flow rates for small watersheds (Kinthada 2014). Hydrologists felt the need to have an analogous procedure that predicts the peak flow rate for larger watersheds. A modification of the 'Rational method' was based on the concept of isochrones. Thus, the modified 'Rational method' was used to solve many of the same type of problems as the original rational method. However, it generally produced more realistic and accurate solutions (Singh et al. 2014).

The unit hydrograph concept was first proposed by Sherman in 1932 based on the principle of superposition for estimating surface runoff in gauged basins(Maddamsetty et al. 2010). This theory has been considered an important contribution to the field of hydrology in deriving flood hydrograph. It was one of the first tools available to hydrologists to predict entire hydrographs instead of just peak discharges (Xiong 2011).

After studying watersheds in the Appalachian Mountains of the United States, Snyder (1938) proposed and developed a set of empirical equations for Synthetic Unit Hydrograph (SUH) for large number of catchments in Appalachian Highland of Eastern United States. Albishi (2016) derived a unit hydrograph of Allith River Basin in the South West of Saudi Arabia and its S-curve in the South Western part of Saudi Arabia for predicting flash flood more accurately in the region.

Gebremeskel et al. (2002) proposed a flood estimation method by combining GIS with distributed hydrologic modeling. This method has mainly focused on discussing a flood hydrograph estimation method by using physiographic characteristics and recorded meteorological data. Elmoustafa et al. (2013) used digital elevation model to delineate watersheds and the morphological parameters to determine flood risk in the Sinai Peninsula, Egypt.

Therefore, the broad inferences that can be drawn from the review of literature are:

a) DEMs are widely accepted for use in drainage pattern extraction.

b) DEMs are very useful for hydrological processing of the catchment, but little has been done for developing hydrograph from the hydrological processing.

c) The Time–Area (TA) technique is believed to perform best for small to intermediate steep watersheds where runoff process is mainly governed by translation.

Hence, an attempt is made in the present study to use DEM for the simulation on a catchment for estimating flood through the preparation of unit hydrograph and validate the model comparing the results with the observed flood discharges.

Objectives of the Study

The present study has been taken up with the following objectives:

- > To prepare a Digital Elevation Model of the study area.
- > To obtain the drainage characteristics of the study area.
- To derive a Peak Runoff Unit Hydrograph for the drainage basin from DEM hydro processing and to estimate peak floods for different storms.
- To validate the peak flood discharge obtained from the computed hydrograph for the total study area.

For this purpose, a part of the Sarada River Basin has been taken as a case study.

Study Area

The Sarada is an East flowing medium sized river located in Visakhapatnam district of Andhra Pradesh on the East Coast of India (Fig 1). The river has a total catchment area of 2,665 km². The 122 km long Sarada River originates at approximately 1000 m elevation in the Anantagiri hills of the Eastern Ghats and flows in a general NW–SE direction for over 62 km up to Anakapalle town, where it abruptly changes its direction to N–S, and finally empties into the Bay of Bengal. Bound by 17°25' and 18°15' North latitudes, and 82°32' and 83°06' East longitudes, the length of the Sarada River Basin is 90 km along its long axis (North to South) and about 55 km at its widest(East to West) in its headwater region. The overall drainage network in the basin appears to be dendritic to sub-dendritic pattern. Being essentially a rain fed river, the water flow in Sarada and its tributaries is highly seasonal and hence it is an ephemeral drainage system. The basin is surrounded by River Nagavali on the North, River Gosthani, Gambhiram Gedda, Meghadri Gedda on the East, Bay of Bengal on the South, Tandava and Eleru River Basins and the Machhkund sub-basin of the River Godavari on the West(Kinthada 2014).



Fig. 1: Location of the Upper Sarada River Basin

There is one river gauge station on the Sarada River located near Anakapalle town (17°41'21.66" N, 82°59'53" E) and maintained by the Central Water Commission (CWC), Government of India. Hence, the present study is restricted to the Upper Sarada River Basin covering the drainage network up to the river gauge point. The Upper Sarada River Basin comprising a catchment area of 1952 km² and bound by 17°41'10" and 18°15' North latitudes, and 82°32' and 83°06' East longitudes. The Sarada River is joined by several tributaries along its left bank, while very few or no main tributaries join it along its right bank. Some of the important tributaries contributing their discharge to the Sarada River along its left bank are: Bodderu Nadi, Tacheru Vagu, Vedurla Gedda, Pedderu and Chintagedda (Fig. 2).



Fig. 2: Drainage Map of the Upper Sarada River Basin

Data Collected

Data on rainfall and river discharges, which provide the important information on the hydrographic conditions of the basin are collected from the governments' records and tabulated here.

Rainfall data

Data on rainfall have been collected from 23 rain gauge stations set up by AP Revenue Department in as many revenue mandals' (tahsils) in and around the Sarada River Basin in Visakhapatnam district. The daily rainfall data recorded at each of these 23 mandals over a 30-year period from 1990 to 2019were obtained from the Directorate of Economics and Statistics (Revenue Department, Visakhapatnam). Fig. 3 shows the location of the rain gauge stations from which the rainfall data was collected. Table 1 shows the mean annual rainfall for each rain gauge station. The rain gauge stations are represented by their ID numbers as given in the Table 1.





Fig. 3: Location of rain gauge stations in the study area. Numbers in parentheses below the names of the rain gauge stations indicate the average annual rainfall in mm recorded at the respective stations.

Table 1: Data on mean annual rainfall from 23 Rain gauge stations in and around UpperSarada River Basin in Visakhapatnam district

C No	Rain Gauge	Names of Rain Gauge	Mean Annual	Longitude	Latitude
5.INO.	Station ID	Stations	Rainfall (mm)	(°E)	(°N)
1	2	KASIMKOTA	1130	82.96	17.66
2	3	ANAKAPALLE	1181	83.00	17.69
3	4	CHODAVARAM	1163	82.94	17.82
4	5	DEVARAPALLE	1188	82.98	17.98
5	6	ANANTHAGIRI	1309	83.00	18.23
6	7	YELAMANCHILI	1114	82.86	17.54
7	8	K KOTAPADU	1198	83.04	17.88
8	9	CHEEDIKADA	1158	82.89	17.92

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9	10	MADUGULA	1359	82.81	17.91
10	11	MAKAVARAPALEM	1174	82.72	17.61
11	12	BUTCHAYYAPETA	1098	82.87	17.78
12	15	MUNAGAPAKA	1106	82.99	17.63
13	19	PEDABAYALU	1310	82.58	18.28
14	20	ROLUGUNTA	1228	82.67	17.71
15	21	NARSIPATNAM	1247	82.61	17.66
16	23	GOLUGONDA	1159	82.47	17.67
17	25	S RAYAVARAM	1112	82.80	17.45
18	26	RAVIKAMATHAM	1190	82.80	17.79
19	27	PADERU	1269	82.67	18.07
20	28	PARAVADA	1131	83.07	17.62
21	29	G MADUGULA	1395	82.53	18.01
22	30	MUNCHINGIPUTT	1623	82.51	18.36
23	31	HUKUMPETA	1237	82.69	18.14

Average Annual Rainfall: 1121 mm

River discharge data

The Sarada River discharge data for the study area from the year 1990 to 2019, recorded by Central Water Commission (CWC), Anakapalle station, was used to select flood events and validation of the predicted flood discharges is done using this data.

METHODOLOGY

The estimation of runoff for a unit net rainfall was done for the selected drainage basin of the study area to prepare a unit hydrograph. In this paper, the Survey of India maps were scanned and geo-coded using UTM (Universal Transverse Mercator) projection, zone 44 and Everest 1956 spheroid. ILWIS software was used to digitise contour maps (with value domain) and drainage maps (with class domain). The streams in the drainage map are designated by Strahler order such as first order, second order, third order, fourth order, etc; whereas contours are denoted with their elevation values (Strahler, 1957). By contour interpolation, DEM was developed and used for processing the drainage extraction. The DEM hydro-processing includes filling of local depressions (fill sinks), creation of flow direction map, flow accumulation map, drainage network extraction and drainage network ordering. The methodology for drainage extraction from DEM is shown in a flowchart (Fig 4).



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Fig. 4: Flowchart of Methodology for drainage extraction from DEM



Fig. 5: Flowchart showing the GIS methodology for Unit Hydrograph preparation The DEM of the selected drainage basin was used to develop a classified slope map. The slope map was classified based on the USGS classification system. As the flow velocity (V) is proportional to the slope (S), i.e., $V = f(S^{1/2})$, the slope map was assigned weightages based on this criterion. Then the weighted map for the drainages was developed. Further, a point map of the outlet to the catchment was prepared, for the use as 'source' to prepare the distance map, which shows the equivalent distances from the outlet, through 'Distance Calculation operation' in ILWIS 3.4. This distance map was converted to a point map, and the point map was opened as a table having point data with coordinates. This point data was imported into the SURFER 10 to develop contours of equal interval showing lines joining the points of equal time of

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concentration from the outlet. These isochrones are then imported to ILWIS 3.4. This map was then digitized to get segment map and was then rasterised. The rasterised contour map was crossed in ILWIS with the flow accumulation map of the extracted drainage map. This yielded the values of the discharge in terms of number of pixels for each time step (isochrones interval). Using this data, the runoff was estimated by taking appropriate assumptions and a unit hydrographwas plotted. An S-hydrograph was plotted to obtain a unit hydrograph of selected time duration for the use in flood estimate due to a storm.

The flowchart showing the methodology used for the preparation of the unit hydrograph is shown in Fig. 5 and the flowchart showing the overall methodology of flood prediction is shown in Fig. 6.



Fig. 6: Flowchart of overall methodology used for flood estimation

The assumptions made to prepare the unit hydrograph (UH) are:

- 1. Entire area is divided into eleven equal time steps (ΔT) based on upstream distance from the outlet.
- 2. Rainfall duration is equal to $11^*\Delta T$.
- Average rainfall is obtained from Thiessen polygon prepared using nearest point method in ILWIS.
- 4. Storm occurred uniformly over the entire catchment.
- 5. Run off coefficient is uniform over the entire catchment.

- 6. Base flow is zero.
- 7. Runoff is dependent on the gradient.

RESULTS & DISCUSSION

Based on the assumption of spatially uniform rainfall of uniform intensity, the peakest runoff unit hydrograph is developed from DEM using GIS analysis for Upper Sarada River Basin (Fig. 7&Table 2). The peakest discharge for the 54.56 hour rainfall giving 1cm direct runoff is found to be 96.88m³/s with basin lag of 27.28 hour.



Fig. 7: Unit Hydrograph for Upper Sarada River Basin

The peak discharge for the one day and 6 hr unit hydrograph obtained from S-hydrograph (Fig.8, Fig. 9&Table 3) was computed to be 91.13 m³/s and 72.89 m³/s, a base period of 104.17& 84.33 hour with a basin lag of 54.56 & 44.64 hour.





S-Hydrograph for total Upper Sarada River Basin





Fig. 9: Computed hydrographs using maximum computed discharge of 6 hr and One-Day duration derived from S–hydrograph for Upper Sarada River Basin

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Isochrones (m)	Time (min)	Q (Npix)	ΔQ (Npix)	Cum ΔQ (Npix)	Flow Area (m ²)	Discharge (m ³ /s)
0	0	0	0	0	0	0
100000	297.62	3044715	125616	125616	78510000	4.00
200000	595.24	2919099	110033	235649	147280625	7.50
300000	892.86	2809066	194225	429874	268671250	13.68
400000	1190.48	2614841	192129	622003	388751875	19.79
500000	1488.1	2422712	347164	969167	605729375	30.84
600000	1785.72	2075548	467476	1436643	897901875	45.71
700000	2083.34	1608072	402775	1839418	1149636250	58.53
800000	2380.96	1205297	504330	2343748	1464842500	74.57
900000	2678.58	700967	376806	2720554	1700346250	86.56
1000000	2976.2	324161	146769	2867323	1792076875	91.23
1100000	3273.82	177392	177392	3044715	1902946875	96.88
	3571.44			2919099	1824436875	92.88
	3869.06			2809066	1755666250	89.38
	4166.68			2614841	1634275625	83.20
	4464.3			2422712	1514195000	77.09
	4761.92			2075548	1297217500	66.04
	5059.54			1608072	1005045000	51.17
	5357.16			1205297	753310625	38.35
	5654.78			700967	438104375	22.30
	5952.4			324161	202600625	10.31
	6250.02			177392	110870000	5.64
	6547.64			0	0	0

Table 2: Peak Run-off computation for Upper Sarada River Basin

T (hrs)	Q (m³/s)	Lag 54.5 hrs	Lag 54.5 hrs	S-H YG	T (hrs)	S-H YG	T (hrs)	S-H YG	T (hrs)	S-H YG	Shift ed by 6hrs	Diff.	T (hrs)	6 hrs UH	T (hrs)	S-H YG	Shift ed by 24hr s	Diff.
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		0
4.96	4	0	0	4	4.96	4	2.48	2	1.24	1	0	1	1.24	1	1.24	1		1
9.92	7.5	0	0	7.5	9.92	7.5	4.96	4	2.48	2	0	2	2.48	2	2.48	2		2
14.88	13.68	0	0	13.68	14.88	13.68	7.44	5.75	3.72	3	0	3	3.72	3	3.72	3		3
19.84	19.79	0	0	19.79	19.84	19.79	9.92	7.5	4.96	4	0	4	4.96	4	4.96	4		4
24.8	30.84	0	0	30.84	24.8	30.84	14.88	13.68	6.2	4.87	0	4.87	6.2	4.87	6.2	4.87		4.87
29.76	45.71	0	0	45.71	29.76	45.71	19.84	19.79	7.44	5.75	0	5.75	7.44	4.75	7.44	5.75		5.75
34.72	58.53	0	0	58.53	34.72	58.53	24.8	30.84	9.92	7.5	1	6.5	9.92	5.5	9.92	7.5		7.5
39.68	74.57	0	0	74.57	39.68	74.57	29.76	45.71	14.88	13.68	2	11.68	14.88	10.68	14.88	13.68		13.68
44.64	86.56	0	0	86.56	44.64	86.56	34.72	58.53	19.84	19.79	3	16.79	19.84	15.79	19.84	19.79		19.79
49.6	91.23	0	0	91.23	49.6	91.23	39.68	74.57	24.8	30.84	4	26.84	24.8	25.96	24.8	30.84	0	30.84
54.56	96.88	0	0	96.88	54.56	96.88	44.64	86.56	29.76	45.71	4.87	40.84	29.76	39.96	29.76	45.71	1	44.71
59.52	92.88	4	0	96.88	59.52	96.88	49.6	91.23	34.72	58.53	5.75	52.78	34.72	51.03	34.72	58.53	2	56.53
64.48	89.38	7.5	0	96.88	64.48	96.88	54.56	96.88	39.68	74.57	7.5	67.07	39.68	60.9	39.68	74.57	3	71.58
69.44	83.2	13.68	0	96.88	69.44	96.88	59.52	96.88	44.64	86.56	13.68	72.88	44.64	66.77	44.64	86.56	4	82.57
74.41	77.09	19.79	0	96.88	74.41	96.88	64.48	96.88	49.6	91.23	19.79	71.44	49.6	60.4	49.6	91.23	4.87	86.36
79.37	66.04	30.84	0	96.88	79.37	96.88	69.44	96.88	54.56	96.88	30.84	66.04	54.56	51.17	54.56	96.88	5.75	91.13
84.33	51.17	45.71	0	96.88	84.33	96.88	74.41	96.88	59.52	96.88	45.71	51.17	59.52	38.35	59.52	96.88	7.5	89.38
89.29	38.35	58.53	0	96.88	89.29	96.88	79.37	96.88	64.48	96.88	58.53	38.35	64.48	22.3	64.48	96.88	13.68	83.2
94.25	22.3	74.57	0	96.88	94.25	96.88	84.33	96.88	69.44	96.88	74.57	22.31	69.44	10.31	69.44	96.88	19.79	77.09
99.21	10.31	86.56	0	96.88	99.21	96.88	89.29	96.88	74.41	96.88	86.56	10.32	74.41	5.64	74.41	96.88	30.84	66.04
104.2	5.64	91.23	0	96.88	104.2	96.88	94.25	96.88	79.37	96.88	91.23	5.65	79.37	0	79.37	96.88	45.71	51.17
109.1	0	96.88	0	96.88	109.1	96.88	99.21	96.88	84.33	96.88	96.88	0			84.33	96.88	58.53	38.35
		92.88	4	96.88			104.2	96.88	89.29	96.88	96.88	0			89.29	96.88	74.57	22.3
		89.38	7.5	96.88			109.1	96.88	94.25	96.88	96.88	0			94.25	96.88	86.56	10.31
		83.2	13.68	96.88					99.21	96.88	96.88	0			99.21	96.88	91.23	5.64
		77.09	19.79	96.88					104.2	96.88	96.88	0			104.2	96.88	96.88	0
		66.04	30.84	96.88					109.1	96.88	96.88	0			109.1	96.88	96.88	0
		51.17	45.71	96.88													96.88	
		38.35	58.53	96.88													96.88	
		22.3	74.57	96.88													96.88	
		10.31	86.56	96.88													96.88	
		5.64	91.23	96.88													96.88	
		0	96.88	96.88													96.88	
			92.88	92.88													96.88	
			89.38	89.38													96.88	
			83.2	83.2													96.88	
			77.09	77.09													96.88	
			66.04	66.04														
			51.17	51.17														

Table 3: Computation of S - Hydrograph, 6 hr UH and 1 Day UH for Upper Sarada River Basin

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	38.35	38.35							
	22.3	22.3							
	10.31	10.31							
	5.64	5.64							
	0	0							

Flood prediction for Selected Storms:

From the available rainfall and river discharge data, eight storm events are selected for validating the models (Fig. 10 to Fig. 17). The peak runoff hydrograph is validated with the observed hydrographs. A comparison of observed and computed peak flood discharges in the study area is given in Table 4.





Observations from graph in Fig. 10 are:

- (i) The maximum observed discharge is $499.70 \text{ m}^3/\text{s}$.
- (ii) The computed peak discharge obtained from one day UH is $517.95 \text{ m}^3/\text{s}$.
- (iii) The computed peak discharge occurred on the Sixth day.
- (iv) The observed peak also occurred on the same day.
- (v) The computed peak discharge exceeded the observed discharge by $18.25 \text{ m}^3/\text{s}$







Observations from graph in Fig. 11 are:

- (i) The maximum observed discharge is $571.10 \text{ m}^3/\text{s}$.
- (ii) The computed peak discharge obtained from one day UH is $603.35 \text{ m}^3/\text{s}$.
- (iii) The computed peak discharge occurred on the Sixth day.
- (iv) The observed peak occurred on the Fifth day.
- (v) The computed peak discharge exceeded the observed discharge by $32.25 \text{ m}^3/\text{s}$



Fig. 12: Hyetograph, flood hydrograph and observed discharge for Upper Sarada River Basin for the storm event during 09thOctober– 20thOctober, 1998.

Observations from graph in Fig. 12 are:

- (i) The maximum observed discharge is $887.00 \text{ m}^3/\text{s}$.
- (ii) The computed peak discharge obtained from one day UH is $955.67 \text{ m}^3/\text{s}$.
- (iii) The computed peak discharge occurred on the Ninth day.
- (iv) The observed peak occurred on the Eighth day.
- (v) Themaximum observed discharge exceeded the computed peak discharge by $68.67 \text{ m}^3/\text{s}$.



Fig. 13: Hyetograph, flood hydrograph and observed discharge for Upper Sarada River Basin for the storm event during 12th October – 24th October, 2005.

Observations from graph in Fig. 13 are:

- (i) The maximum observed discharge is $572.67 \text{ m}^3/\text{s}$.
- (ii) The computed peak discharge obtained from one day UH is $662.37 \text{ m}^3/\text{s}$.
- (iii) The computed peak discharge occurred on the Fifth day.
- (iv) The observed peak occurred on the Fourth day.
- (v) The computed peak discharge exceeded the observed discharge by $89.70 \text{ m}^3/\text{s}$.





Observations from graph in Fig. 14 are:

The maximum observed discharge is $850.50 \text{ m}^3/\text{s}$.

- (i) The computed peak discharge obtained from one day UH is 911.65 m^3/s .
- (ii) The computed peak discharge occurred on Fifth day.
- (iii) The observed peak occurred on the Eighth day.
- (iv) The computed peak discharge exceeded the observed discharge by $61.15 \text{ m}^3/\text{s}$.



11thOct - 23rd Oct' 2014 UPPER SARADA RIVER BASIN

Fig. 15: Hyetograph, flood hydrograph and observed discharge for Upper Sarada River Basin for the storm event during 11thOctober– 23rdOctober, 2014.

Observations from graph in Fig. 15 are:

- (i) The maximum observed discharge is $767.85 \text{ m}^3/\text{s}$.
- (ii) The computed peak discharge obtained from one day UH is $1295.53 \text{ m}^3/\text{s}$.
- (iii) The computed peak discharge occurred on Fourth day.
- (iv) The observed peak occurred on the Third day.
- (v) The computed peak discharge exceeded the observed discharge by $527.68 \text{ m}^3/\text{s}$.



18th Sep - 28th Sep' 2016 UPPER SARADA RIVER BASIN



Observations from graph in Fig. 16 are:

- (i) The maximum observed discharge is $487.45 \text{ m}^3/\text{s}$.
- (ii) The computed peak discharge obtained from one day UH is $527.49 \text{ m}^3/\text{s}$.
- (iii) The computed peak discharge occurred on Sixth day.
- (iv) The observed peak occurred on the Ninth day.
- (v) The computed peak discharge exceeded the observed discharge by $40.04 \text{ m}^3/\text{s}$.







Observations from graph in Fig.17 are:

- (i) The maximum observed discharge is $257.54 \text{ m}^3/\text{s}$.
- (ii) The computed peak discharge obtained from one day UH is $345.40 \text{ m}^3/\text{s}$.
- (iii) The computed peak discharge occurred on Ninth day.
- (iv) The observed peak occurred on the Same day.
- (v) The computed peak discharge exceeded the observed discharge by $87.87 \text{ m}^3/\text{s}$.

Table 4: Comparison of observed and computed peak flood discharges in the Upper Sarada

	Peak Flood Discharges						
Period	Observed (cumecs)	Computed(One Day UH in cumecs)					
03 rd Oct to 13 th Oct 1992	499.70	517.95					
06 th Oct to 19 th Oct1995	571.10	603.35					
09 th Oct to 20 th Oct1998	887.00	955.67					
12 th Oct to 24 th Oct 2005	572.67	662.37					
20 th Oct to 31 st Oct 2013	850.50	911.65					
11 th Oct to 23 rd Oct 2014	767.85	1295.53					
18 th Sep to 28 th Sep 2016	487.45	527.49					
29 th Sep to 11 th Oct 2017	257.54	345.40					

River Basin

The flood estimates obtained from unit hydrograph for selected storm events are found to higher than the observed values and it can be concluded that it may be due to improper

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infiltration values which are randomly assumed for the spatially varying rainfall and uniform intensity and are not valid for these storms

CONCLUSION

The conclusions drawn from the above study are presented as follows:

The drainage network map with threshold value 500 is found more relevant with original drainage map obtained from 1:50,000 SOI map in terms of the number of stream and lengths of streams of each order. The flood estimates made for different events of consecutive rainy days in the study area using the peakest flood unit hydrograph are validated with the observed discharges recorded by CWC. It can be concluded that the flood estimates are in a close agreement with the observed values except in some cases which may be due to the reason that assumed rainfall duration (24 hours) and uniform intensity are not valid for these storms. The effect of the three reservoirs built across the Sarada River, namely Raiwada, Konam & Pedderu are responsible for the flood estimate to be higher than the observed values which need to be studied further.

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